

MODELING AND CONTROL OF AIRBORNE WIND ENERGY SYSTEMS USING LIFTING LINE/SURFACE AERODYNAMICS

J.-B. Crismer, F. Trigaux, M. Duponcheel, G. Winckelmans

Institute of Mechanics, Materials and Civil Engineering, UCLouvain, 1348 Louvain-la-Neuve, Belgium



www.uclouvain.be/immc



jean-baptiste.crismer@uclouvain.be

1 ► CONTEXT AND MOTIVATION

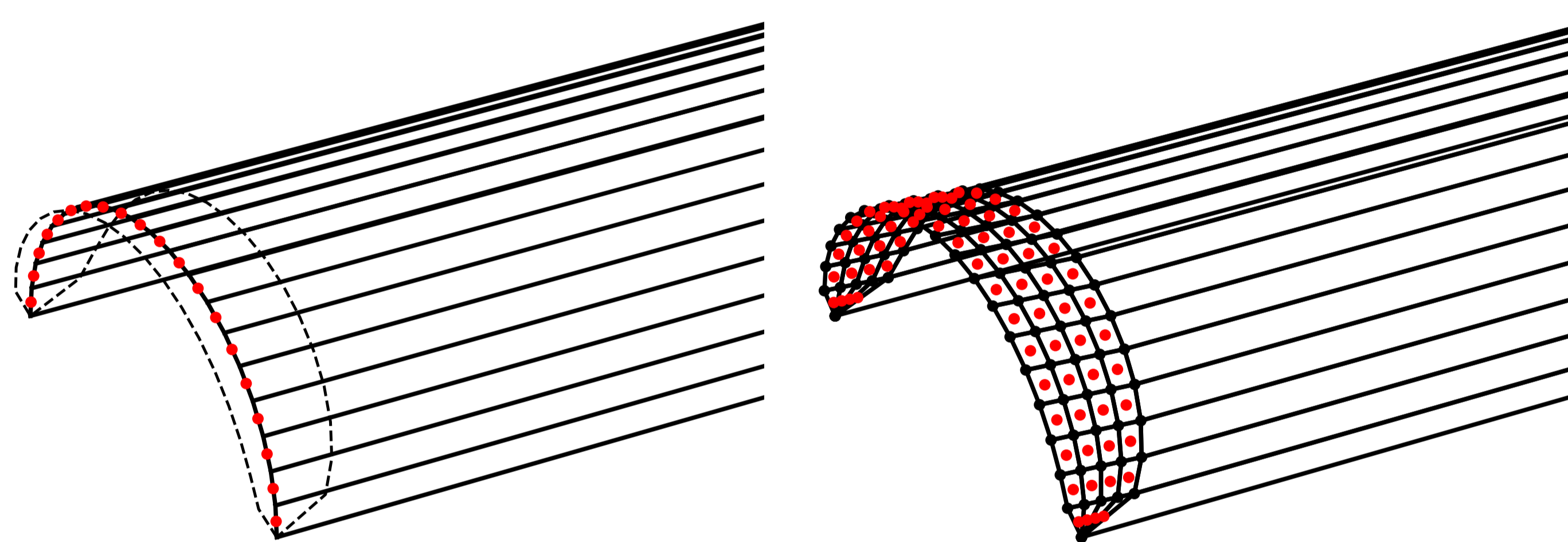
Airborne Wind Energy Systems have complex aerodynamic behaviors. Such devices also operate in perturbed flows (turbulent ABL, wakes, ...). They therefore need **accurate aerodynamic models**.

Lifting line and lifting surface:

- Good representation of wing aerodynamics
- Computationally cheap
- Allow to represent both fixed wings and soft wings
- Flow perturbations scales smaller than the wing span can be taken into account

2 ► METHODOLOGY

Lifting line/surface models are built using **horseshoe vortices** and **vortex rings** assemblies [1].

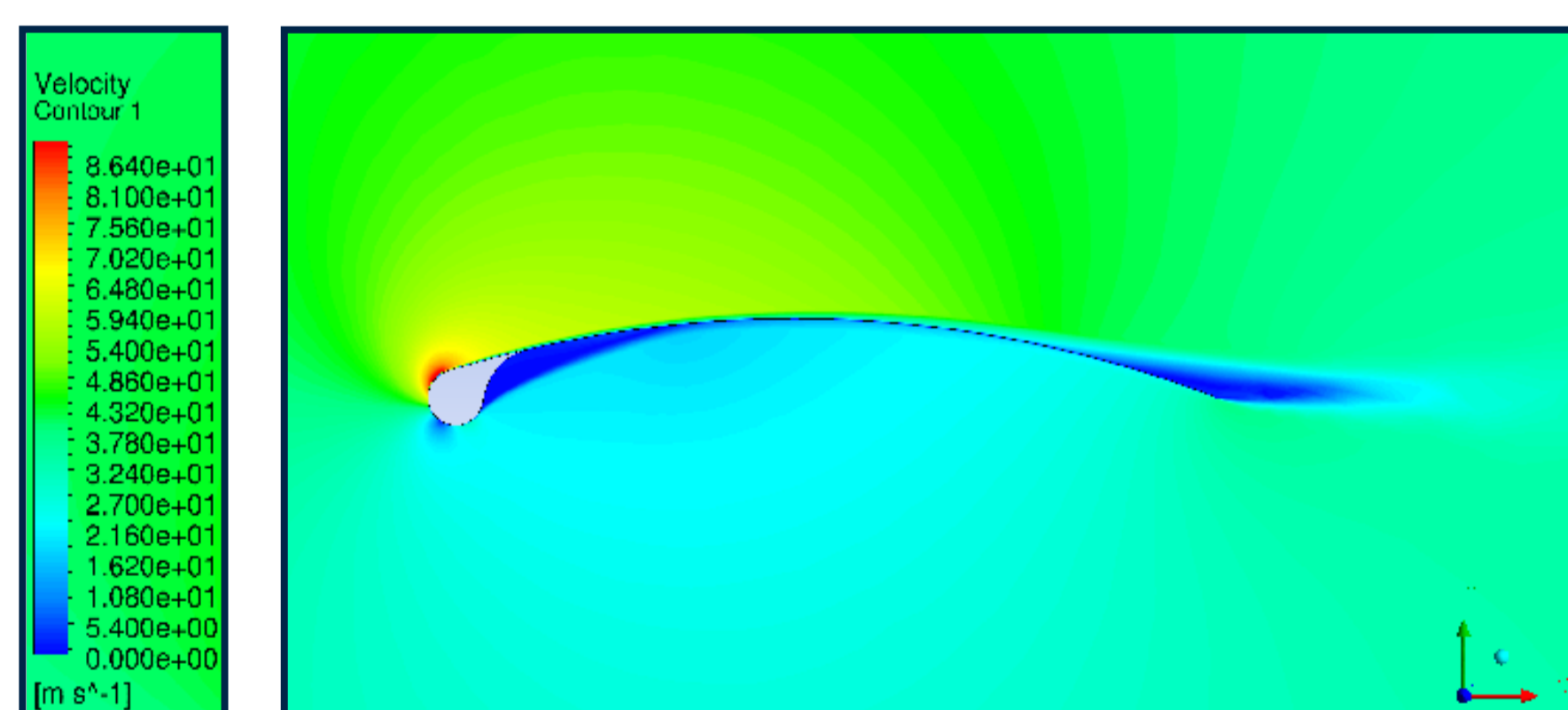


Lifting line method

Lifting surface method

The induced velocity is evaluated for each vortex segment using the Biot-Savart law.

The implemented **lifting line** is a numerical extension of the Prandtl lifting line method [2]. It can be implemented in a non linear way to allow the use of **polar curves** [3]. Kite airfoil polar curves (lift, drag and moment coefficients) are obtained from experiments or are generated using RANS. The effect of unsteady aerodynamics can also be implemented.



RANS of a Leading Edge Inflatable (LEI) kite airfoil at 10° angle of attack: norm of the velocity field.

The **lifting surface** best represents low aspect ratio wings (such as kites). The method also captures the **chordwise load distribution**.

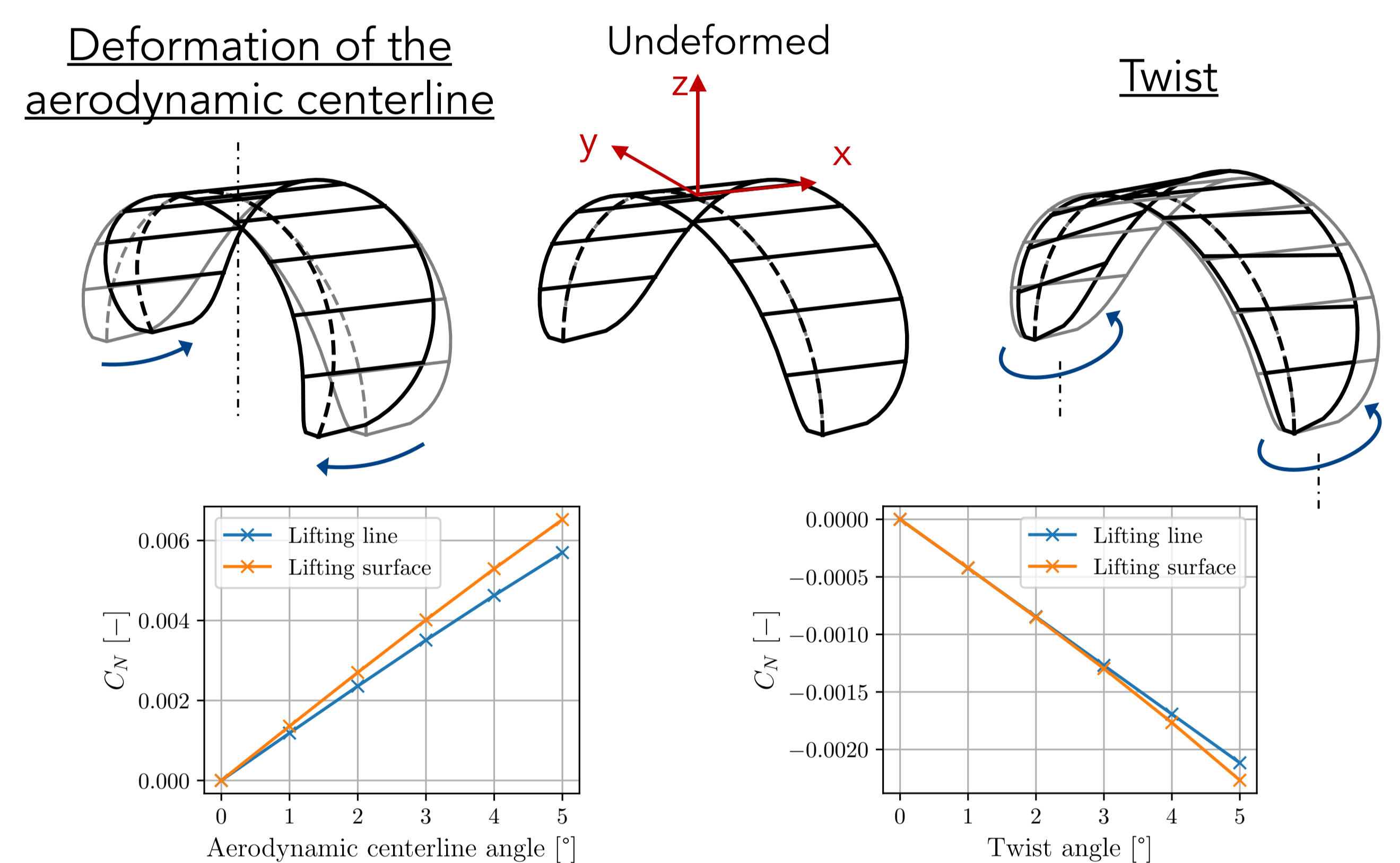
Polar curves cannot be used but **geometrical complexities** can be taken into account (such as large deformations, camber effects, etc.).

3 ► SOFT WING DEFORMATION

Two **deformation** modes are identified to be responsible for control of a kite in **yaw** [4]:

- **Twist** of the airfoil profiles along the span
- **Deformation** of the **aerodynamic centerline**

The steering capabilities of the two modes are studied. Both deformations are applied linearly along the span (no deformation at the center of the wing and maximal deformation at the tips).

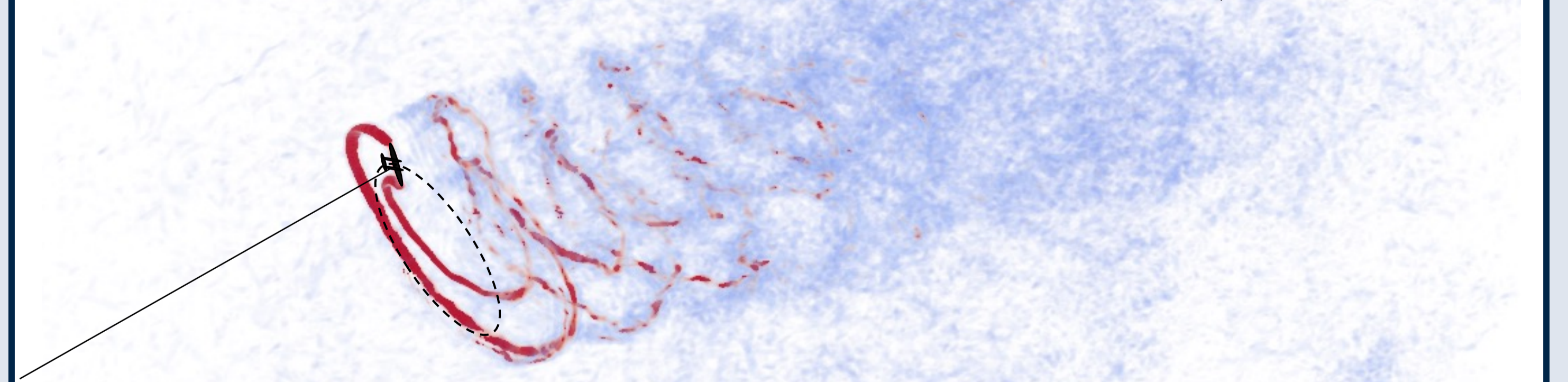


Yawing moment coefficient due to the two deformation modes

The variation of the moment coefficient with the angle is obtained for each mode considered independently.

4 ► PERSPECTIVES

- Further understanding of the **steering behavior** in relation to the deformation modes
- Coupling of the aerodynamic models (lifting line, lifting surface) with **AWES dynamics and control**
- Study of AWES aerodynamics and control in **flows with perturbations** (encounter of wake vortices, of gusts) and in **turbulent flows** (ABL)
- Implementation of the methods in a **LES framework** (using actuator line/curve and actuator surface methods)



LES of a fixed wing AWES in a flow at $U_\infty = 10$ m/s with 6% TI

5 ► REFERENCES AND ACKNOWLEDGMENTS

- [1] J. Katz and A. Plotkin. Low speed aerodynamics. Cambridge University Press, 2001.
- [2] R. Leloup, Roncin K., G. Bles, J. Leroux, C. Jochum, and Y. Parlier. Estimation of the lift-to-drag ratio using the lifting line method: application to a leading edge inflatable kite. Airborne Wind Energy, 2013.
- [3] J.D. Anderson. Fundamentals of aerodynamics. McGrawHill, 5th edition, 2011.
- [4] J. Breukels.: An Engineering Methodology for Kite Design. Ph.D. Thesis, Delft University of Technology, 2011.

This work is carried out as part of the BORNE project, funded by the Energy Transition Funds from the SPF Economy. BORNE (Belgian Offshore aiRborne wind Energy): Developing the tools and insight to expand the Belgian offshore wind farms with airborne wind energy systems.

Computational resources have been provided by the Consortium des Équipements de Calcul Intensif (CÉCI), funded by the Fonds de la Recherche Scientifique de Belgique (F.R.S.-FNRS) under Grant No. 2.5020.11 and by the Walloon Region.